

Apparatus for High-Pressure High-Temperature X-Ray Powder Diffraction Studies

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A high-pressure high-temperature x-ray powder diffraction apparatus has been developed based on a modification of the belt apparatus, which is an internally heated compressible gasket device. The unique feature of this device is that the die-support ring assembly is fabricated in two parts which mate along a plane normal to the piston axis. The split-die design permits entry of the x-ray beam into the high-pressure volume and egress of both the diffracted rays and the undeviated beam through suitable grooves and fan-shaped slots ground in the mating surfaces. The high-pressure x-ray windows are either a beryllium ring with a wedge-shaped cross section or epoxy resin stops at the bore of the die. The high-pressure medium is "amorphous" boron, and the sample is in the form of a thin cylinder which is coaxial with the pistons and normal to the x-ray beam. The compressible gaskets between the pistons and the die are made of pyrophyllite, as they are in conventional devices, inasmuch as they are not part of the x-ray path. High sample temperatures are attained by resistance heating of carbon rods adjacent to the sample. Present limitations on pressure and temperature are 100 kilobars and 1000°C. High-intensity Mo K α radiation is employed. The apparatus is portable and may be positioned on a conventional x-ray source.

INTRODUCTION

ONE of the potentially most promising areas of high-pressure research which is relatively unexplored is that of structural studies on crystalline solids at pressures in excess of 20 kilobars at sustained temperatures in excess of 300°C. Such studies could provide basic data on the equation-of-state, nonquenchable phase transitions, order-disorder phenomena, etc. of solids.

At present there are three basic designs being used for high-pressure x-ray diffraction measurements. The diamond cell¹⁻³ consists of a pair of diamonds in the configuration of Bridgman anvils and the x-ray beam is transmitted through the diamonds perpendicular to the anvil faces and the sample plane. Carbide Bridgman anvils are used for⁴⁻⁶ x-ray diffraction measurements with the x-ray beam transmitted parallel to and between the anvil faces. The third design utilizes the tetrahedral high-pressure apparatus⁷ to generate pressure and the x-ray beam is transmitted in and out of the high-pressure volume through the compressible gaskets. For high-pressure studies at elevated temperature the first two designs are restricted by the effect of external heating on the properties of the carbide or diamond anvils (less than 500°C). The tetrahedral device can be internally heated and is limited only by the combination of requirements fixed by the gasket material, i.e., low x-ray absorption, proper frictional qualities to effect a high-pressure seal, and high-temperature stability.

The apparatus described in this article utilizes a belt-type high-pressure cell⁸ with a split die for entrance and egress of x rays from the high-pressure region. The essential feature of this design is the separation of the x-ray beam path from the compressible gasket region in an internally heated high-pressure high-temperature device. This permits the use of standard gasketing materials, such as pyrophyllite, to effect the pressure seal irrespective of their x-ray absorption characteristics. This design has been used to 1000°C and 100 kilobars.

APPARATUS

The high pressure is generated in a modified high-compression belt of the type developed by Bundy.⁹ The high-pressure volume is 0.25 cm high by 0.5 cm in diameter, which is large enough for internal heating to over 1000°C. Fifty tons of ram force applied to the pistons produces over 100 kilobars internal pressure, so the whole assembly, 50-ton press, die, pistons, and binding rings, can be constructed with a total weight of less than 34 kg. The device, therefore, is portable and can be installed on an x-ray source. Figure 1 is a picture of the high-pressure apparatus aligned with the x-ray source, and Fig. 2 is a schematic representation of this assembly.

To provide entry for the x-ray beam and exit of both the diffracted rays and the undeviated beam, the die and the support ring assembly of the high-compression belt were fabricated in two halves which mate in a plane perpendicular to the piston axis. The entrance and exit ports are ground into the mating surfaces of the two halves (Fig. 3). The die halves (5 cm diam, 1.25 cm thick) are made of Carpenter-Hampton tool steel hardened to 60-62 R_c, and the binding rings (10 cm o.d., 5 cm i.d., 1.25 cm thick) are made of Vascojet 1000 hardened to 50 R_c. The die and binding ring halves fit together with 1° taper and 0.028 cm

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¹ M. J. Piermarini and C. E. Weir, *J. Res. Nat. Bur. Stand. (U. S.)* **66A**, 325 (1962).

² B. L. Davis and L. H. Adams, *Phys. Chem. Solids* **25**, 379 (1964).

³ W. A. Bassett, T. Takahashi, and P. W. Stook, *Rev. Sci. Instrum.* **38**, 37 (1967).

⁴ J. C. Jamieson and A. W. Lawson, *J. Appl. Phys.* **33**, 776 (1962).

⁵ E. A. Perez-Albuerne, K. F. Forsgen, and H. G. Drickamer, *Rev. Sci. Instrum.* **35**, 29 (1964).

⁶ D. B. McWhan and W. L. Bond, *Rev. Sci. Instrum.* **35**, 626 (1964).

⁷ J. D. Barnett and H. T. Hall, *Rev. Sci. Instrum.* **35**, 175 (1964).

⁸ H. T. Hall, *Rev. Sci. Instrum.* **31**, 125 (1960).

⁹ F. P. Bundy, *J. Chem. Phys.* **38**, 631 (1963).